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Transient terahertz photoconductivity measurements of minority-carrier lifetime in tin sulfide thin films: Advanced metrology for an early stage photovoltaic material

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Materials research with a focus on enhancing the minority-carrier lifetime of the light-absorbing semiconductor is key to advancing solar energy technology for both early stage and mature material platforms alike. Tin sulfide (SnS) is an absorber material with several clear advantages for manufacturing and deployment, but the record power conversion efficiency remains below 5%. We report measurements of bulk and interface minority-carrier recombination rates in SnS thin films using optical-pump, terahertz-probe transient photoconductivity (TPC) measurements. Post-growth thermal annealing in H₂S gas increases the minority-carrier lifetime, and oxidation of the surface reduces the surface recombination velocity. However, the minority-carrier lifetime remains below 100 ps for all tested combinations of growth technique and post-growth processing. Significant improvement in SnS solar cell performance will hinge on finding and mitigating as-yet-unknown recombination-active defects. We describe in detail our methodology for TPC experiments, and we share our data analysis routines in the form of freely available software. © 2016 AIP Publishing LLC. [<http://dx.doi.org/10.1063/1.4940157>]

I. INTRODUCTION

Solar cells need long-lived electronic excitations to deliver a useful amount of power. The minority-carrier lifetime of the light-absorbing semiconductor is a crucially important metric to evaluate an absorber material. This is firmly established for technologies based on Si wafers, for which lifetime measurements are routine. Minority-carrier lifetime is equally as important for thin-film solar cells based on materials other than Si, but measurements are not routine and are frequently inaccurate. Accurate lifetime metrology accelerates the technological development of materials and is a valuable screening metric for new materials.¹ Here we report measurements of minority-carrier lifetime in SnS thin films using optical-pump, terahertz (THz)-probe transient photoconductivity (TPC) measurements. SnS is an absorber with important advantages for solar cell manufacturing, but the record power conversion efficiency remains below 5%.² We demonstrate the impact of annealing and surface treatments on the bulk and surface minority-carrier recombination rates, and we illustrate the effect of minority-carrier recombination rates on solar cell performance. Throughout we highlight the challenges of measuring minority-carrier lifetime in thin films and we demonstrate methods to overcome these challenges.

In Section II, we motivate the importance of minority-carrier lifetime and introduce SnS as a solar cell absorber. In Section III, we describe the sample set and procedures to

control bulk and surface recombination rates. In Section IV, we present the results and compare to solar cell device performance. In Section V, we discuss details of the measurement and data analysis. Section VI contains discussion and conclusions. Experimental details particular to SnS can be found in Section III, and details related to the measurement technique can be found in Section V.

II. THE IMPORTANCE OF MINORITY-CARRIER LIFETIME FOR SOLAR CELLS. INTRODUCTION TO SnS

Long minority-carrier lifetime is essential for high performance solar cells. The precise lifetime required to ensure high performance depends on the optical absorption length and excess-carrier mobility, and the minority-carrier lifetime by itself is a crude figure of merit. Nevertheless, a long lifetime is important. In Figure 1(a), we compile reports of minority-carrier lifetime and solar cell efficiency for different thin film absorber materials: CdTe, Cu(In,Ga)(S,Se)₂ (CIGS), Cu₂ZnSnS₄ (CZTS), MAPbX₃ (methylammonium lead halide “perovskites”), InP, GaAs, and SnS. We show only data for which both lifetime and device measurements were reported for samples that were synthesized in the same laboratory and using as close to the same synthesis procedure as is reasonably possible. The data in Figure 1 come from a variety of experimental techniques; for accurate comparisons, we encourage the reader to consult the original sources.

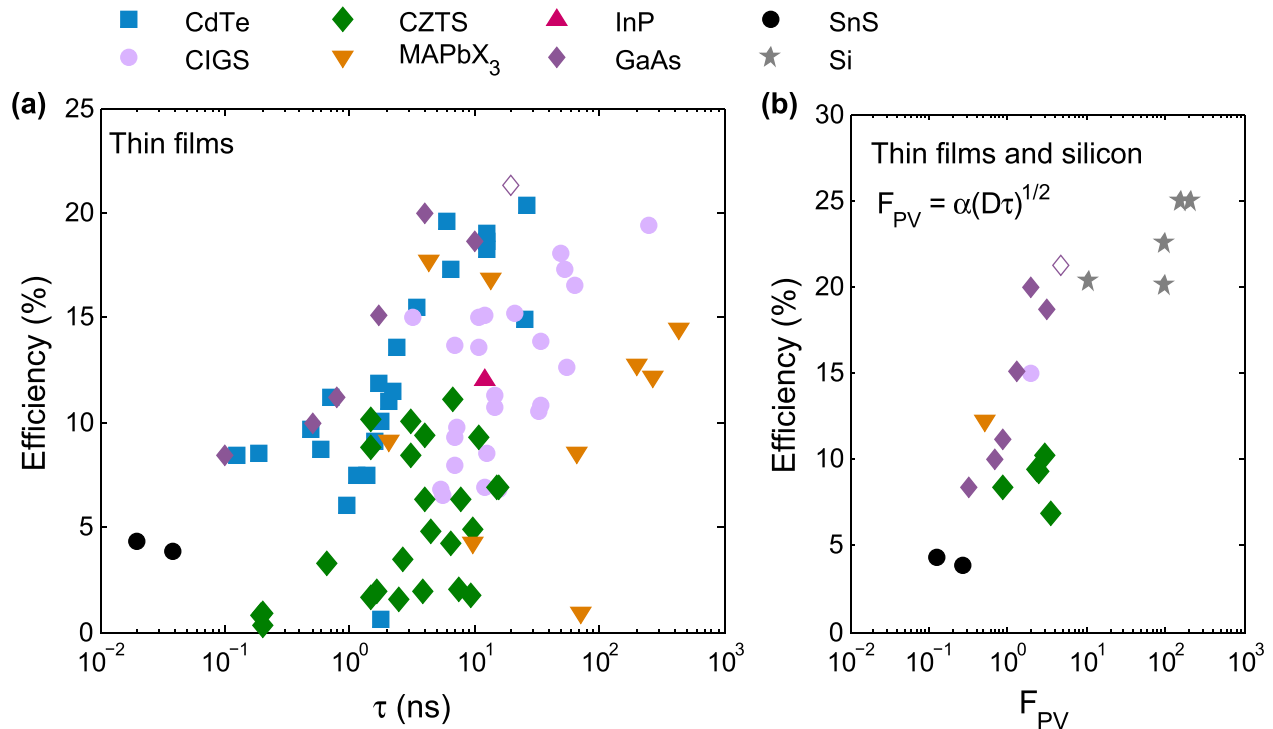


FIG. 1. Minority carrier lifetime (τ) and a solar cell figure of merit (F_{PV}) vs device efficiency. Efficiency values are for AM1.5 insolation. (a) Minority-carrier lifetime vs device efficiency for thin film absorbers. (b) Figure of merit (F_{PV}) vs device efficiency for thin films and crystalline silicon wafers. In (a), we only show data for which both τ and device measurements were performed on samples that were synthesized in the same laboratory and using as close to the same procedure as is reasonably possible; in (b), we additionally require that D and α are reported on comparable samples, with the exception of silicon and GaAs. For silicon and GaAs, we use tabulated values for D and α . For SnS, the efficiencies are as reported in Refs. 2 and 3. For GaAs, all data represent heteroepitaxial growth except for the hollow point, which represents homoepitaxial GaAs-on-GaAs. For other materials, the sources of data are: CdTe, Refs. 35–37 and 62; CIGS, Refs. 39–42; CZTS, Refs. 42–46; MAPbX₃, Refs. 27–31; InP, Refs. 63 and 47; GaAs, Refs. 38 and 64–66; Si, Refs. 48–50 and 67.

Although it is possible to make a poorly performing solar cell from high lifetime material, the converse seems to be impossible. Figure 1(a) includes the lifetime measurements on SnS that compare directly to our previously published efficiency marks of 3.88% and 4.36% and that are described in Sections III and IV.^{2,3}

Most of the materials presented in Figure 1(a) have bandgaps appropriate for single-junction solar cells, can absorb the majority of above-bandgap light in 1 μm thick films, and are typically incorporated into solar cells as polycrystalline thin films. Within this set of technologically relevant constraints, the minority-carrier lifetime is a valuable figure of merit. The minority-carrier lifetime in silicon can exceed 100 μs for Czochralski-grown wafers, orders of magnitude higher than thin film materials.⁴ However, this is compensated by the fact that the optical absorption depth in candidate thin film materials is orders of magnitude shorter than in silicon. The minority-carrier lifetime is too crude a metric to capture these differences.

For a more sophisticated solar cell figure of merit, we consider the dimensionless ratio (F_{PV}) of minority-carrier diffusion length to optical absorption length

$$F_{PV} = \alpha\sqrt{D\tau}. \quad (1)$$

D is the minority carrier diffusivity, τ is the bulk minority-carrier lifetime, and α is the optical absorption coefficient. In

Figure 1(b), we present compiled data for F_{PV} and solar cell efficiency, including results for wafer-based silicon technologies. With the exception of silicon, all of the materials represented strongly absorb light at energies above their respective bandgaps. For each material, we calculate F_{PV} using α as measured at the knee the curve of $\log_{10}(\alpha(E))$. With the exception of Si and GaAs, we require that lifetime, diffusivity, absorption coefficient, and device measurements were reported for samples that were synthesized in the same laboratory and using as close to the same procedure as is reasonably possible. For crystalline silicon, we assume the values $\alpha = 300 \text{ cm}^{-1}$ and $D = 36$ and $12 \text{ cm}^2 \text{ s}^{-1}$ for electrons and holes, respectively. For GaAs, we assume the values $\alpha = 10^4 \text{ cm}^{-1}$ and $D = 200$ and $10 \text{ cm}^2 \text{ s}^{-1}$ for electrons and holes, respectively.

Due to its large diffusivity, GaAs can support high device performance even for relatively short minority carrier lifetime (Figure 1(a)). However, GaAs must be grown epitaxially and with very large grains to support high performance. Of the results presented in Figure 1(a), GaAs are the only data points that represent epitaxial films. We show mostly data for hetero-epitaxial GaAs films grown on substrates such as multicrystalline Ge and graded-composition SiGe because this approach compares most closely to the other thin film technologies presented here. One data point for homoepitaxial GaAs-on-GaAs is shown for comparison.

For the materials presented in Figure 1(a), it is widely assumed that the minority carrier lifetime is limited by defect-

assisted recombination. In our analysis of SnS results, we make the same assumption.

SnS is an absorber with several inherent advantages compared to materials that are widely used in solar cells, but its demonstrated efficiency is too low for commercial relevance. It is composed of non-toxic, Earth-abundant, and inexpensive elements. SnS is an inert and water-insoluble semiconducting mineral (Herzenbergite) with an indirect bandgap of 1.1 eV, strong light absorption for photons with energy above 1.4 eV ($\alpha > 10^4 \text{ cm}^{-1}$), and intrinsic *p*-type conductivity with carrier concentration in the range 10^{15} – 10^{17} cm^{-3} .^{5–7} SnS evaporates congruently and is phase-stable up to 600 °C.^{8,9} This means that SnS thin films can be deposited by thermal evaporation and its high-speed cousin, closed space sublimation (CSS), as is employed in the manufacture of CdTe solar cells. It also means that SnS phase control is simpler than for most thin film PV materials, notably including CIGS and CZTS. Therefore, efficiency stands as the primary barrier to commercialization of SnS solar cells. However, this efficiency barrier cannot be overstated. The record efficiency for SnS solar cells is 4.36% (certified), and simulations indicate that the device performance is limited by minority-carrier lifetime.¹⁰ For SnS solar cells to improve, research must focus on increasing the minority-carrier lifetime, and reliable lifetime metrology is indispensable.

III. THE SnS THIN FILM SAMPLE SET. BULK ANNEALING AND SURFACE PASSIVATION

Previous work has shown that SnS solar cells are improved by post-growth annealing and by surface oxidation.^{2,3,11} Annealing in H₂S gas leads to improvements in short circuit current density (J_{SC}), fill factor (FF), and open circuit voltage (V_{OC}). Creating a thin SnO₂ layer in between the SnS absorber and the *n*-type buffer layer improves V_{OC} . These results suggest that H₂S annealing reduces the bulk defect density and improves the minority-carrier lifetime, and that surface oxidation passivates

defects and reduces the surface recombination velocity (SRV). These hypotheses are supported by the observation that H₂S annealing promotes secondary grain growth, and that oxygen point defects at an SnS interface remove dangling bond states from the bandgap.^{6,12} The solar cell studies have been performed on devices in the substrate configuration, so that the *p*-type absorber is deposited before the *n*-type buffer layer. The fabrication sequence is: SnS deposition, H₂S annealing, surface oxidation, and buffer layer deposition.

We vary the annealing and surface oxidation treatments of SnS films grown by thermal evaporation and atomic layer deposition (ALD) and measure the effect on the bulk lifetime and the SRV. The films grown by thermal evaporation are 1000 nm thick and are grown using the same chamber and growth conditions as those used in the devices reported in Refs. 3 and 13. The films grown by ALD are 380 nm thick and are grown using the same chamber and growth conditions are those used in the devices reported in Refs. 2 and 13. The substrate temperature during growth is 240 and 200 °C for thermal evaporation and ALD, respectively. The outstanding difference between the films studied here and the films used in devices is that these films are grown on fused quartz for compatibility with the THz absorption measurement, whereas for solar cells, the films are grown on Mo. The different annealing and oxidation treatments studied are summarized in Table I.

We measured the minority carrier lifetime (τ_0) and SRV (S) with optical-pump, THz-probe TPC. τ_0 indicates the low-injection limit of the minority-carrier defect-assisted recombination lifetime (Section VE). Each sample was measured with at least two combinations of pump wavelength and fluence in order to increase the confidence in the estimated bulk and surface recombination rates. Several samples were measured repeatedly in two different laboratories. τ_0 and S were estimated for each sample by global fits to multiple data sets. In Figure 2, we show representative data and fits for a single sample (TE4). The experiments and data analysis are described in detail in Section V.

TABLE I. SnS thin film sample set for lifetime measurements. TE is the thermal evaporation, ALD is the atomic layer deposition. All samples are grown on fused quartz substrates. Previous results suggest that H₂S annealing improves the bulk minority-carrier lifetime, and that oxidation of the surface lowers the SRV. For sample TE5, the Zn(O,S):N composition is the same as used in the previously published devices.^{2,3,13}

Sample name and number	Growth	H ₂ S annealing	Surface treatment
TE1 (SnS141016p)	TE	None	<15 s air exposure
TE2 (SnS140901e)	TE	None	24 h air exposure
TE3 (SnS140901a)	TE	Short anneal (28 Torr, 4% H ₂ S in N ₂ , 400 °C, 1 h)	24 h air exposure
TE4 (SnS140901d)	TE	Long anneal (80 Torr, 2% H ₂ S + 2% H ₂ in N ₂ , 450 °C, 3 h, with 2 h linear controlled cooldown)	24 h air exposure
TE5 (SnS141016n)	TE	Short anneal	Air exposure, then Zn(O,S):N (1 super cycle, approximately 3 nm thick)
TE6 (SnS141016o)	TE	Short anneal	Air exposure, then UV/ozone exposure (5 s)
TE7 (SnS140901h)	TE	None	Air exposure, then O ₂ plasma (10 W, 0.5 Torr, 12 s)
TE8 (SnS140901f)	TE	None	Air exposure, then H ₂ O ₂ exposure (5 cycles of 2.1 Torr s, for a total of 10.5 Torr s)
TE9 (SnS140901b)	TE	Short anneal	Air exposure, then H ₂ O ₂ exposure
ALD1 (Solar093B)	ALD	None	H ₂ O ₂ exposure
ALD2 (Solar093D)	ALD	Short anneal (10 Torr, 99.5% H ₂ S, 400 °C, 1 h)	H ₂ O ₂ exposure

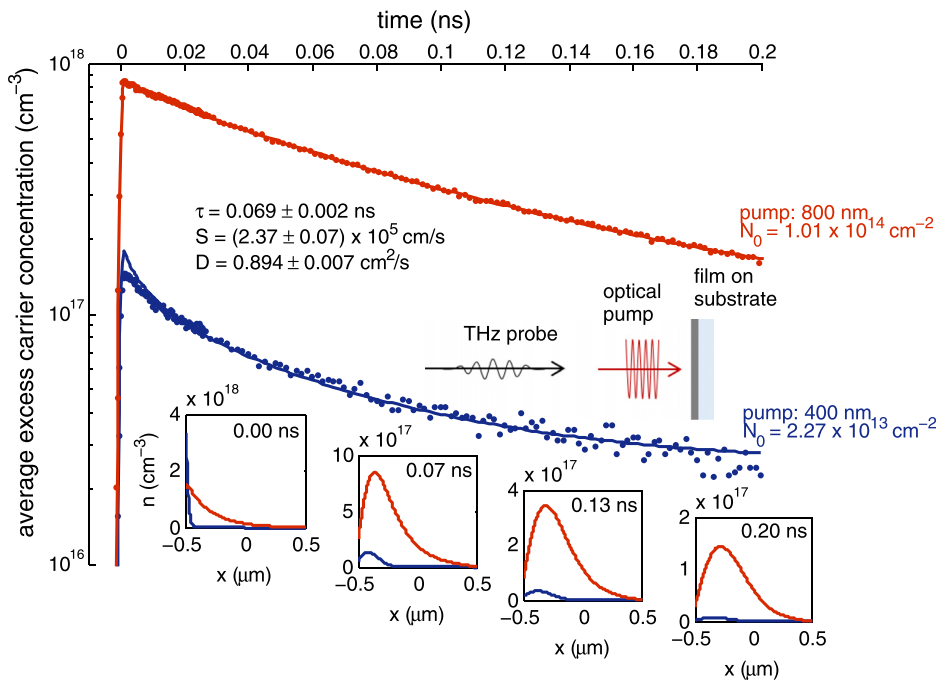


FIG. 2. TPC data and fits for a single sample (TE4). The sample was measured with 800 nm (red) and 400 nm (blue) pump wavelengths. Points are data, and lines are the fitted model. Both data sets were fit simultaneously to determine τ , S , and D . The main axis shows $\bar{n}(t)$, the excess minority-carrier concentration averaged through the sample thickness. The insets show $n(x)$, the spatial distribution of the excess-carrier concentration, at four points in time according to the fitted model. The schematic illustration shows the film-on-substrate sample structure, the tunable optical pump pulse, and the THz probe pulse.

IV. RESULTS: BULK AND INTERFACE MINORITY-CARRIER RECOMBINATION IN SnS THIN FILMS, AND COMPARISON TO SOLAR CELL PERFORMANCE

In Figure 3, we plot the minority-carrier lifetime (τ_0) and SRV (S) for the full sample set. Sample TE3 corresponds to the solar cell devices made from thermally evaporated SnS and reported in Refs. 3, 9, and 13. For this sample, $\tau_0 = 38 \pm 1$ ps and the diffusion length $L_D = \sqrt{\tau_0 D_e} = 54.7 \pm 0.5$ nm, where D_e is the minority-carrier diffusivity. This can compare with the value $L_D = 86 \pm 22/17$ nm that was estimated using a device model to fit quantum efficiency data measured on finished devices.⁹ The trends in the results for τ_0 and S across our whole sample set support the hypothesis introduced

above, that annealing in an H_2S atmosphere increases τ_0 , and that oxidation of the surface decreases S .

Annealing in H_2S increases τ_0 for both thermally evaporated and ALD films. Samples TE3 and TE5 correspond closely to the process used to fabricate the 3.88% device reported in Refs. 3 and 13. This so-called “baseline” process includes H_2S annealing of the thermally evaporated SnS film, followed by oxidation in ambient air, followed by deposition of the Zn(O,S,N) buffer layer. Compared to the baseline process, sample TE4 was annealed for a longer time in higher H_2S partial pressure and at higher temperature, resulting in a larger τ_0 . Sample TE2 was not annealed and has a smaller τ_0 relative to the baseline process. The progression

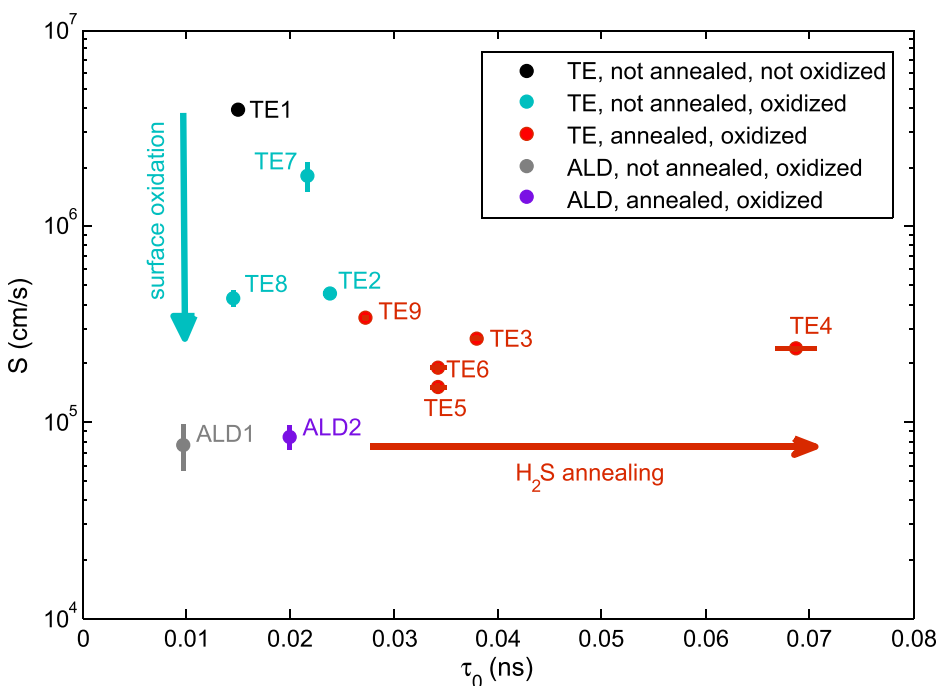


FIG. 3. Minority-carrier lifetime (τ_0) and SRV (S) for the full sample set described in Table I. Error bars indicate the 95% confidence intervals of the global fits. The arrows summarize the trends in the data and confirm our hypotheses based on previous studies of completed solar cells.

of increasing τ_0 from samples TE2, to TE3, to TE4 shows the effect of H_2S annealing. Similarly, τ_0 increases going from non-annealed sample TE8 to annealed sample TE9, where both samples received the same H_2O_2 exposure. The ALD samples are also consistent with this trend, with the annealed sample (ALD2) having a larger τ_0 than the non-annealed sample (ALD1). Annealing SnS films in H_2S results in secondary grain growth, and we hypothesize that the increased minority-carrier lifetime results from a reduction in the density of extended crystallographic defects.⁶

Oxidation passivates the SnS surface and reduces S . This is seen by comparing samples TE1 and TE2. Sample TE2 was oxidized by exposure to ambient air for 24 h, and $S = 4.5 \pm 0.3 \times 10^5 \text{ cm s}^{-1}$. In contrast, the air exposure for sample TE1 was kept to a minimum: it was exposed to ambient for less than 10 s in total in between growth in high-vacuum ($<10^{-7}$ Torr) and measurement in a medium-vacuum ($<10^{-1}$ Torr). For this sample, $S = (3.9 \pm 0.3) \times 10^6 \text{ cm s}^{-1}$. Samples ALD1 and 2 have the lowest SRV, with an average value $S = (8 \pm 1) \times 10^4 \text{ cm s}^{-1}$. These samples were oxidized by H_2O_2 exposure immediately after growth, without intervening exposure to ambient air. We hypothesize that the lowering of S by oxidation is due to the partial substitution of sulfur by oxygen, which is predicted to move dangling bond electronic states out of the bandgap.¹²

Although oxidation passivates the surface, an aggressive process is counterproductive. Sample TE7 was exposed to an O_2 plasma and the resulting SRV is extremely high. We hypothesize that ion bombardment in the O_2 plasma reactor creates more recombination-active defects than oxidation eliminates.

H_2O_2 exposure of thermally evaporated films that were previously air-exposed increases the minority carrier recombination rates. For films that are not annealed, H_2O_2 exposure decreases τ_0 (compare TE2 and TE8). For the annealed samples, H_2O_2 exposure decreases τ_0 and slightly increases S (compare TE3 and TE9). This is surprising, since the SnS solar cell efficiency record is held by a device grown by ALD and including surface passivation by H_2O_2 , as for sample ALD2. However, the thermally evaporated films were exposed to air before the H_2O_2 treatment, whereas the ALD-grown films were not (this is consistent with the fabrication procedure for the reported solar cell devices).¹³ We hypothesize that the chemically aggressive H_2O_2 damages the previously formed oxide at free and internal interfaces. The samples are polycrystalline, and certain physical processes may affect both S and τ_0 . For example, a process that creates defects on the surface may also create defects on the internal grain boundaries. Such a process would increase S and reduce τ_0 . It appears that H_2O_2 exposure of thermally evaporated, air-exposed films is such a process.

In Figure 4(a), we compare τ_0 to the power conversion efficiency (η) of solar cell devices made from films with the same growth and processing procedures. We plot η as measured in our laboratory, and the error bars indicate the distribution of measurements on multiple devices. For these measurements, light-masking was not used, and the spectrum of the solar simulator was not frequently calibrated.

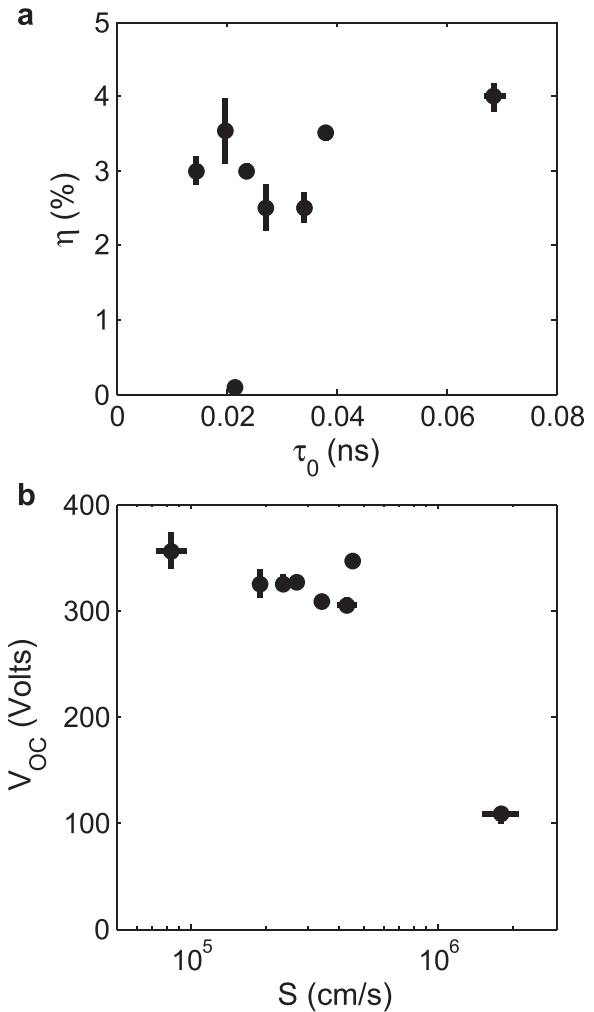


FIG. 4. Dependence of SnS solar cell device performance on minority-carrier recombination. (a) η vs τ_0 . Due to the relatively small range of τ_0 across our sample set, the effect of changing τ_0 is easily masked by competing factors. (b) V_{OC} vs S . Error bars for τ_0 and S indicate the 95% confidence intervals of the global fits. Error bars for η and V_{OC} represent the standard error for tests on multiple devices; for all data points at least 4 devices were measured.

Therefore, these results are less accurate than the certified data reported in Refs. 2 and 3 and reproduced in Figure 1. We observe a slight rising trend in η with τ_0 . Relatively small changes in τ_0 are difficult to correlate to device performance because there are many factors that affect η : as Figure 1 demonstrates, a large τ_0 is a necessary but not sufficient condition for a high performance solar cell.

The open-circuit voltage (V_{OC}) is often strongly affected by surface recombination. The recombination current density is larger at V_{OC} than at any other point in the power-generating quadrant of the current-voltage curve. Furthermore, at V_{OC} the absorber is close to flat-band conditions. As a result, the product (pn) of majority and minority-carrier concentrations is enhanced at the interface. In Figure 4(b), we compare S and V_{OC} . There is a clear trend of decreasing V_{OC} with increasing S . We do not observe a clear trend in V_{OC} vs τ_0 (not shown). This implies that at V_{OC} , the interface contributes more to the total recombination current density than does the quasi-neutral region.

V. TRANSIENT PHOTOCONDUCTIVITY MEASUREMENTS OF MINORITY-CARRIER LIFETIME IN THIN FILMS

Minority-carrier lifetime is determined by measuring the excess concentration of minority-carriers that results from optical excitation.^{14,15} By “excess” we mean a state away from thermal equilibrium. Unfortunately, the quantity measured is not the excess minority-carrier concentration, but a function of the same. Photoluminescence measures the rate of optical recombination, and photoconductivity measures the electrical conductivity; both are functions of the excess majority- and minority-carrier concentrations. The spatial profile of excess-carriers through the sample is rarely measured but can be modeled with assumptions. For wafer-based materials such as Si, the experimental methodologies and the assumptions involved are mature, and the results are often accurate.^{14,16} For thin films, these same methodologies and assumptions are usually inappropriate. The parameter space for measurements of thin films is very different than for wafers, and for most thin film materials, the unknowns are more numerous and problematic.

Here we discuss seven aspects of our experimental procedure and data analysis:

- Key assumptions: defect-assisted recombination and absence of electric fields
- Optical-pump, THz-probe transient photoconductivity measurements: Description of the experiments
- Optical-pump, THz-probe transient photoconductivity measurements: Data pre-processing
- The spatial profile of excess-carriers
- Measurements under high-injection conditions
- The challenge of unknown diffusivity
- Sample heating and other phenomena that affect the data at long times

These details arise in the case of optical-pump, THz-probe measurements on SnS thin films, but the methods discussed may apply to a wide range of materials and to related techniques.

A. Key assumptions: Defect-assisted recombination, and absence of electric fields

We assume that the minority-carrier lifetime is limited by defect-assisted recombination, and that the competing processes radiative recombination and Auger recombination do not affect the lifetime. This is applicable to the majority of thin film solar cells. Optical recombination is significant only for solar cells based on single crystals of direct bandgap semiconductors such as GaAs.¹⁷ Auger recombination is significant for solar cells that operate at very high injection levels or have high bulk doping densities, such as certain types based on monocrystalline Si.¹⁸ The Auger and defect-assisted recombination rates are equal for injection level $n_A = \sqrt{1/\Gamma\tau}$, where Γ and τ are the Auger coefficient and defect-assisted recombination lifetime, respectively. For $n \ll n_A$ Auger recombination is irrelevant. Γ is unknown for SnS so we use the value for Si, $\Gamma = 1 \times 10^{-30} \text{ cm}^6 \text{ s}^{-1}$. For the values of τ reported here $n_A > 10^{20} \text{ cm}^{-3}$ and $n \ll n_A$ is

satisfied for all of the data. Γ varies by at most a factor of five between Si and different main group metal chalcogenide semiconductors such as PbS and PbSe. Therefore, we assume that this estimate using Γ for Si is applicable to SnS. Auger recombination would also manifest as a sub-linear dependence of the peak measured injection (\bar{n}_{MAX}) on the pump fluence N_0 , which we do not observe for either 400 or 800 nm pump wavelength (Appendix C).

We assume that there are no electric fields in the film, either in equilibrium or under illumination. Our samples are bare thin films grown on fused quartz and are capped by ultra-thin (<5 nm) oxide layers, so it is reasonable to assume that there are no heterojunctions and associated electric fields. We assume that there is no surface voltage due to trapped charge at the surface. Finally, we assume that charge moves by ambipolar diffusion such that no space charge develops during the measurement. This assumption may be unjustified in some cases. However, it is essential in order to restrict the model to diffusive dynamics, instead of coupled drift-diffusion and electrostatics. This makes the problem tractable for curve-fitting with a personal computer and widely available software. The accuracy of assuming ambipolar diffusion may be assessed by comparing the dielectric relaxation time to the minority-carrier lifetime. The relaxation time τ_r is equal to $\epsilon_0\epsilon_r/\sigma$ where $\epsilon_0\epsilon_r$ and σ are the static dielectric susceptibility and electrical conductivity, respectively.¹⁹ For short times $t < \tau_r$ (t is the time elapsed since the optical pump), electrons and holes diffuse independently with different diffusion coefficients. The resulting accumulation of space-charge results in an electric field and a Debye potential. For long times $t > \tau_r$ the space-charge is screened and electrons and holes diffuse together with the ambipolar diffusion coefficient. τ_r is difficult to estimate for SnS. ϵ_r is anisotropic and has not been measured at low frequency. Density functional theory predicts that ϵ_r ranges from 34 to 52 depending on orientation.²⁰ The DC conductivity that we measure is affected by grain-boundary scattering, whereas τ_r is controlled by the intra-granular mobility. Measurements of mobility in single-crystal SnS range from 10 to well over $1000 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$.^{21,22} Our own THz spectroscopic measurements of the complex dielectric response of a bare SnS film at equilibrium find $\sigma = 1.0 \pm 0.8 \text{ S/cm}$ and $\epsilon_r = 29 \pm 1$ at 1 THz, in reasonable agreement with the aforementioned published results. Using these values, we estimate that $\tau_r = 1\text{--}10 \text{ ps}$. This implies that ambipolar diffusion is an accurate assumption for all but the initial time points in our experiments, and that the excess-carrier dynamics should be little affected by electric fields due to different hole and electron diffusivities.

B. Optical-pump, THz-probe transient photoconductivity measurements: Description of the experiments

In a TPC experiment, excess-carriers are generated by a short pulse of above-bandgap light, and the relaxation to equilibrium is measured by the absorption of long-wavelength light. The optical pump and the THz probe are generated from an amplified femtosecond laser source and are separated in time by a delay line. Two different optical

pump wavelengths ($\lambda = 400$ and 800 nm) are used in this experiment to generate excess-carriers at different depths. The THz signal is measured in transmission through the film-on-substrate sample. The bandwidth of the THz measurement is approximately 2 THz. The experimental setup is described fully in Ref. 23.

For the TPC experiments, we measure the amplitude of the transmitted electric field (T) at a fixed position in the THz waveform as a function of pump-probe delay time (t) and compare this signal to the amplitude transmission (T_0) in the absence of a pump. T_0 is measured at least 1 ms after the most recent optical pump. The raw data are $(T(t) - T_0)/T_0 \equiv \Delta T/T_0$. The amplitude transmission is measured at the peak of the THz waveform. We have explicitly confirmed that there is negligible phase change due to the presence of the SnS film. This is consistent with our time-domain THz spectroscopy measurements of a film at equilibrium that show that the “crossover frequency” $f_c > 2$ THz, or equivalently that the Drude scattering time is less than 80 fs. Therefore, the complex conductivity of the film at the THz frequencies used is predominantly real.²⁴

The sample is held either in air, in a box purged with nitrogen gas, or in a cryostat under vacuum, depending on the desired amount of air-exposure. All measurements are performed at room temperature. The spot size of the optical pump is between 2 and 3 mm (radius at 1/e intensity), and the THz probe is between 0.7 and 0.8 mm. We assume that the excess-carrier concentration is laterally uniform as probed by the THz beam. The pump time envelope is 100–200 fs (full-width at half-maximum), and the THz envelope is 500–700 fs. For transient measurements, we do not analyze the THz waveform, and therefore the time resolution is comparable to the THz envelope. We account for finite time resolution by modeling the pump as a Gaussian in time and fitting the initial rise of the data to determine the width of the pulse. For all data reported here the width is 500–700 fs (standard width). The fluence (N_0) of the pump pulse is measured independently and is not a free parameter in the fits. N_0 is the time-integrated fluence for a single pulse in units of photons/area. The pump area is calculated for a circle with radius equal to the experimentally measured radius at which the intensity falls by a factor of 1/e from the maximum. For all data reported here N_0 is between 2×10^{13} and 6×10^{14} cm⁻². The spatial generation profile through the film is determined by the optical absorption coefficient (α) which we measured independently: $\alpha(\lambda = 400 \text{ nm}) = 7.27 \times 10^5$ cm⁻¹ and $\alpha(\lambda = 800 \text{ nm}) = 4.84 \times 10^4$ cm⁻¹. The front surface reflectivity is measured independently and accounted for. Due to the large optical absorption coefficient, reflection at the rear surface does not make a significant contribution to the generation profile. The generation profile is further described in Appendix B.

C. Optical-pump, THz-probe transient photoconductivity measurements: Data pre-processing

In order to extract useful semiconductor device parameters, $\Delta T/T_0$ needs to be converted into excess-carrier concentration. Our films are at most 1 μm thick and the optical wavelength at 1 THz is approximately 300 μm . Therefore,

we use the equation for the amplitude transmission through an air/thin film/substrate structure.²⁵ This equation can be rewritten as

$$\frac{-\Delta T/T_0}{1 + \Delta T/T_0} = f(n_S, d, \sigma_0, m_h^*/m_e^*, p_0) \bar{n}(t). \quad (2)$$

n_S is the substrate index of refraction, d is the film thickness, σ_0 is the equilibrium film conductivity at THz frequencies, and p_0 is the equilibrium majority carrier concentration. m_h^* and m_e^* are the hole and electron effective masses, respectively. $\bar{n}(t)$ is the excess minority-carrier concentration; the bar indicates an average through the film. Please see Appendix A for a description of the function f and the assumptions made. We use Equation (A2) to calculate $\bar{n}(t)$ from $\Delta T/T_0$.

D. The spatial profile of excess-carriers

Low-frequency probes such as infrared (IR), THz, and DC measure the average conductivity through the film, and the terms that appear in Equation (2) are averages through the film. However, the spatial distribution of excess-carriers is rarely uniform, and due to competing processes, the instantaneous decay rate $r(t) = d \log(\bar{n})/d\bar{n}$ depends on the spatial distribution. The spatial distribution approaches a flat line (i.e., becomes independent of position) only when the minority-carrier lifetime is much longer than the diffusion time and the surfaces are not recombination-active. In order to accurately estimate the recombination rates, the excess-carrier spatial profile should be considered. Here we discuss a model for the spatial distribution of excess-carriers, and we explore the parameter spaces within which the spatial distribution must be explicitly considered in order to interpret experiments.

The dynamics of excess-carriers are governed by diffusion, drift, generation, and recombination. We assume spatial uniformity in the plane of the sample, so that all quantities vary only along the out-of-plane axis (x). As described above we neglect drift currents. The generation-diffusion-recombination equation and the boundary conditions are introduced in Appendix B. Solutions to this equation have been discussed extensively in the context of TPC measurements of semiconductor wafers.^{16,26} Solutions have the form

$$n(x, t) = e^{-t/\tau} \sum_j (A_j e^{-\alpha_j^2 D t} \cos(\alpha_j x) + B_j e^{-\beta_j^2 D t} \sin(\beta_j x)). \quad (3)$$

$n(x, t)$ is the excess minority-carrier concentration as a function of space and time, D is the diffusivity, and τ is the bulk minority-carrier lifetime. The frequencies α_n and β_n depend on D , S , and d , and the amplitudes A_j and B_j depend on the spatial distribution of generation. When calculating the average $\bar{n}(t)$, the sine term disappears. The surface recombination rates $\alpha_j^2 D \equiv r_{s,j} \equiv 1/\tau_{s,j}$ characterize the process of carriers diffusing to the surfaces and recombining there. The frequencies satisfy $\alpha_1 < \alpha_2 < \alpha_3 < \dots$. At short times, several frequencies contribute to the measured signal and $\bar{n}(t)$ exhibits a multi-exponential decay. For times $t \gg \tau_{s,2}$ only

the fundamental frequency contributes, and $\bar{n}(t)$ exhibits single-exponential decay with effective lifetime τ_{eff} (Ref. 26)

$$\frac{1}{\tau_{\text{eff}}} = \frac{1}{\tau} + \alpha_1^2 D \approx \frac{1}{\tau} + \left(\frac{d^2}{\pi^2 D} + \frac{d}{2S} \right)^{-1}. \quad (4)$$

Experiments on wafers of highly developed materials usually extend to $t \gg \tau_{s,2}$, in which case τ_{eff} is easily determined by a single exponential fit to the data. In this case, the spatial distribution of excess-carriers does not affect the measurement of τ_{eff} . However, this condition may not be met for thin films.

In Figure 5, we show calculated $\bar{n}(t)$ and $n(x, t)$ for two representative cases. Figure 5(a) shows the case of a long minority-carrier lifetime ($\tau = 125$ ns) and a small diffusivity ($D = 0.15$ cm²/s), typical of MAPbX₃.^{27–31} Figure 5(b) shows the case of a short minority-carrier lifetime ($\tau = 0.03$ ns) and a larger diffusivity ($D = 1$ cm²/s), typical of SnS. For the long-lifetime material, the higher-order frequencies $j > 1$ decay quickly relative to τ_{eff} , and τ_{eff} can be estimated easily from an exponential fit to the data at long times. The spatial distribution of excess-carriers approaches a cosine half-cycle and the shape becomes fixed in time. In contrast, for the short-lifetime material, the higher order frequencies do not decay quickly relative to τ_{eff} . The spatial distribution of excess-carriers changes continually and does not reach the half-cosine shape within a typical experimental time window. In this case, the spatial distribution must be explicitly modeled in order to estimate τ_{eff} .

In Appendix B, we introduce a quantitative criterion to determine when the spatial distribution of excess-carriers must be explicitly modelled, and we evaluate this criterion for particular thin film solar cell absorbers. We also discuss

the quantitative relationship between τ and τ_{eff} and present parameter maps to aid with interpreting measurements of τ_{eff} .

E. Measurements under high-injection conditions

Most solar cells operate at low injection conditions, meaning that the excess-carrier concentration under solar illumination remains lower than the equilibrium majority carrier concentration. Due to limited experimental sensitivity, minority-carrier lifetime measurements are sometimes performed under high-injection conditions. Minority-carrier recombination rates depend on the injection level due to the statistics of trap occupation.³² Under the simple assumption of a mid-gap trap state, the minority-carrier lifetime (τ) can be written as

$$\tau(n) = \tau_0 \frac{1 + 2(n/p_0)}{1 + (n/p_0)}. \quad (5)$$

τ_0 is the minority-carrier lifetime at low injection. Equation (5) shows that the minority-carrier lifetime can be overestimated if measurements are performed under high-injection without appropriate corrections. Introducing Equation (5) means that the generation-diffusion-recombination equation becomes nonlinear and we need to solve it numerically instead of using the linear, analytic solutions.

Equation (5) expresses a basic assumption about the nature of the dominant recombination-active defect. We assume that the defect state is near the middle of the bandgap, and that it can assume only two charge states. We assume that the semiconductor is either *n*- or *p*-type, not intrinsic. Finally, we assume that the recombination lifetime at low injection is the same (τ_0) for both minority and majority carriers. These assumptions are justifiable for SnS, for

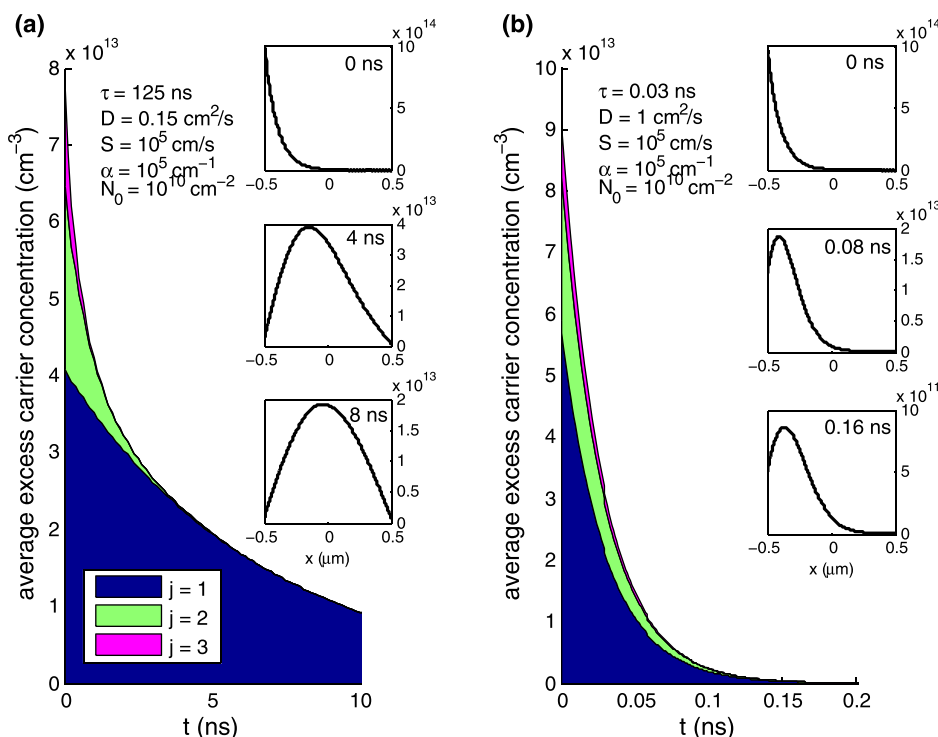


FIG. 5. Decay of spatial frequencies in a TPC experiment, calculated using the solution developed in Ref. 16 and described by Equation (3). The main panels show stacked plots of the first three spatial frequencies ($j = 1, 2, 3$) that contribute to $\bar{n}(t)$. The insets show the spatial distribution $n(x)$ at discrete times. (a) Material with long minority-carrier lifetime and small diffusivity, typical of MAPbX₃. (b) Material with short minority-carrier lifetime and larger diffusivity, typical of SnS. For both simulations $S = 10^5$ cm/s, the optical absorption coefficient (α) is 10^5 cm⁻¹ and the film thickness is $1 \mu\text{m}$. The pump is a delta function pulse of light at $t = 0$ with fluence $N_0 = 10^{10}$ cm⁻². The solution is linear in N_0 , so that a different choice of N_0 would simply scale the vertical axes without affecting the dynamics or the spatial distributions.

which little is known about the recombination-active defects. For better characterized materials, Equation (5) could be easily refined without changing the overall approach.

In Appendix C, we further explore the effect of accounting for injection-dependent minority carrier lifetime, and we discuss the impact on carrier concentration on the surface recombination velocity.

F. The challenge of unknown diffusivity

For wafer-based materials such as Si, the majority- and minority-carrier diffusivity are well characterized and can be treated as known quantities for TPC analysis. This is not the case for thin films. For our films, we only know the in-plane majority carrier Hall mobility, and we rely on assumptions to relate this to required quantities: the in-plane THz-frequency mobilities that appear implicitly in Equation (2), and the out-of-plane diffusivity that appears in the generation-diffusion-recombination equation. We use three tactics to handle these unknowns. First, we assume that all diffusion is ambipolar so that the diffusivity D depends on the excess-carrier concentration, the effective masses, and the majority carrier mobility. Second, we assume that the in-plane and out-of-plane diffusivities are equal. Finally, we use a global fitting routine to simultaneously optimize the model to multiple data sets.

The assumption that there are no electric fields in the film requires that excess majority- and minority-carriers diffuse together. Using the standard expression for the ambipolar diffusion coefficient introduces an additional non-linear term (in addition to the injection-dependent lifetime, see Section VE) to the generation-diffusion-recombination equation. In Appendix D, we introduce the ambipolar diffusion coefficient and explore the effect of injection-dependent diffusivity on the excess carrier model.

The effects of diffusion and surface recombination on $\bar{n}(t)$ are correlated. The diffusivity controls how quickly carriers move towards a surface, and the SRV controls how quickly they recombine once they arrive at the surface. The covariance between D and S becomes extremely large if both are allowed to vary while fitting the generation-diffusion-recombination model for $\bar{n}(t)$ to experimental data, and it is necessary to impose additional constraints in order to draw useful conclusions from the data. To this end, we constrain the in-plane mobility at THz frequencies to be related by the Einstein relation to the out-of-plane diffusivity. Therefore, the fitting parameter D_e , the minority carrier diffusivity in the low-injection limit, affects the overall scale of the dataset in addition to affecting the TPC decay dynamics (see Appendix D). This serves as an additional constraint on the free parameters and reduces the covariance between D and S .

The assumption that in-plane and out-of-plane mobilities are equal is peculiar for a layered, non-cubic material such as SnS. However, X-ray diffraction data show that our films grown on glass or SiO₂ have a distribution of orientations and are not simply oriented along the long axis.³³ The area measured by the TPC experiments is larger than 0.1 cm² and the individual crystal grains have lateral dimension on

the order of 100 nm. The measurement averages over billions of crystal grains, thereby justifying the assumption of equal in-plane and out-of-plane mobility on this scale. For more uniformly oriented samples, additional assumptions could be used to relate the in-plane THz-frequency mobility to the out-of-plane diffusivity.

Finally, we use a global fitting routine to further constrain the free parameters and to reduce covariance between D and S . By fitting simultaneously to multiple data sets, we can constrain certain parameters to be constant across different data sets. For a given sample we hold S , τ_0 , and D_e constant while fitting to data sets with varying the pump wavelength and fluence. For samples that were measured repeatedly in two different laboratories, both sets of measurements were included in the same global fit.

G. Sample heating and other phenomena that affect the data at long times

At long times, the data $\Delta T/T_0$ are expected to decay exponentially to zero with time constant τ_{eff} . However, our data instead saturate at a finite value $(\Delta T/T_0)_{\text{SAT}}$ (see Appendix E). We hypothesize that $(\Delta T/T_0)_{\text{SAT}}$ does not reflect the processes of excess-carrier recombination that we address here, and does not depend in a straightforward way on τ_0 and S . There are two sets of evidence to support this hypothesis. One is the observation that the model described above does not fit the data well unless $(\Delta T/T_0)_{\text{SAT}}$ is explicitly removed or separately accounted for. This is particularly true for global fits to multiple data sets with varying pump wavelength and fluence. At long times, the model predicts an exponential decay with time constant τ_{eff} . If allowed to fit the raw data including $(\Delta T/T_0)_{\text{SAT}}$, the model finds unrealistically large values of τ_0 , well in excess of 1 ns, that depend strongly on the pump. $(\Delta T/T_0)_{\text{SAT}}$ may reflect long-lived electronic excitations in the SnS film such as slow carrier detrapping at grain boundaries or shallow defects, and such phenomena would affect solar cell device performance by limiting the carrier mobility. However, such phenomena are not directly related to the minority-carrier lifetime τ_0 for defect-assisted recombination of minority-carriers in the conduction band. The second line of evidence in support of our hypothesis that non-zero $(\Delta T/T_0)_{\text{SAT}}$ does not depend on τ_0 and S is that transient heating can plausibly account for the observations. In Appendix E, we discuss heating of the film by the laser pulse.

VI. DISCUSSION AND CONCLUSION

Figure 1(a) makes clear that τ_0 of SnS thin films must increase by 100-fold in order for SnS solar cells to join CdTe, CIGS, MAPbX₃, and GaAs as a high-performing thin film solar cell technology. Thermal annealing in H₂S gas helps, but we only achieve increases by a factor of two for the conditions studied here. It remains to be seen whether more intensive annealing conditions (higher H₂S pressure, higher temperature, longer time) will yield further increases in τ_0 . Elsewhere we have reported evidence that τ_0 increases upon raising the film growth substrate temperature, and this is another promising avenue for research.⁹ Unfortunately,

growth and annealing at higher temperature are made difficult by the high vapor pressure of solid SnS. CSS allows the deposition of high vapor pressure materials at high substrate temperatures and is an enabling process for the manufacture of CdTe thin film solar cells. We suggest that growth of SnS thin films by CSS at substrate temperatures above 300 °C, and perhaps in H₂S carrier gas, may yield films with significantly higher τ_0 .

By varying the growth technique and the post-growth treatment, we have attempted to control intrinsic recombination-active defects such as grain boundaries, extended intra-granular crystallographic defects, and intrinsic point defects. However, the fact that all of our samples are clustered at low values of τ_0 suggests that an unknown, extrinsic defect may be polluting the entire sample set. The purity of the precursor chemicals used here is 99.99 at. % for both thermal evaporation and ALD. These are low purity levels for semiconductor synthesis. An impurity with concentration 0.01 at. % in the precursors could be present at concentrations up to approximately 10^{18} cm^{-3} in the films. If such impurity forms a recombination-active defect, then this would dominate the minority-carrier recombination and would frustrate attempts to increase τ_0 by controlling intrinsic defects. We suggest that synthesizing SnS thin films using semiconductor-grade chemical precursors and in a suitably clean growth environment may yield films with significantly higher τ_0 .

The technique described above builds upon decades of research into minority carrier lifetime metrology.^{14,15} Broadly speaking, there are three decisions to make when measuring minority carrier lifetime. The first is the choice of signal to measure. The common choices are photoluminescence or photoconductivity, although other signals such as photoabsorption and photoreflection have been reported.^{27,34} For an indirect bandgap semiconductor such as SnS, photoconductivity yields a stronger signal than photoluminescence. THz photoconductivity, IR free-carrier absorption, and microwave photoconductivity (μ -PC) are related techniques that determine minority-carrier lifetime by measuring the low-frequency photoconductivity.¹⁵ THz- and IR-based techniques offer more information than μ -PC because the low-frequency dielectric response spectrum can be analyzed. μ -PC tends to offer superior signal to noise due to the use of resonant cavities.

The next choice is to measure under transient or steady-state conditions. Transient measurements are preferred for materials with fast recombination processes. Most results on thin film materials employ transient measurements.^{27-31,35-47} Steady-state measurements are common for silicon and have been reported for InP.⁴⁷⁻⁵⁰

The last choice is how to model the excess carrier dynamics. Here we assume that the dynamics can be modeled by the optical generation, ambipolar diffusion, and defect-assisted recombination. The addition of carrier drift is necessary to model processes in samples with a depletion region or with a large Demmer potential. Modeling drift is particularly important for analyzing data on samples with p-n junctions, such as completed solar cells.⁵¹ For very high injection levels, Auger recombination should be considered.⁵²

We are making freely available software that implements the analysis described in Sections V D–V G in an easy-to-use graphical format in the Matlab environment.⁵³ It also allows global fits to multiple data sets with flexible choices of fixed and free parameters. Here we use this global fitting routine to fit the model to multiple data sets collected from individual samples. However, it could also be used to fit the model to data collected from separate samples. This would enable a more flexible form of hypothesis testing. For example, it would be possible to test the hypothesis that certain post-growth oxidation procedures affect S but not τ_0 by comparing goodness-of-fit metrics.

Minority-carrier lifetime is one of the most important figures of merit for a solar cell absorber and is no less important than frequently discussed metrics such as the bandgap, optical absorption, and phase stability. However, unlike most other metrics, minority-carrier lifetime depends strongly on materials processing and can vary by orders of magnitude for a single material composition (Figure 1). Lifetime metrology is therefore key to developing solar cell technology, both for established materials and for early stage materials alike. The difficulty of lifetime metrology on thin films compared to wafer-based materials should not prevent research targeted at improving τ_0 in thin films. Lifetime metrology can be used to assess the impact of materials processing more quickly and with greater accuracy than the fabrication and test of complete solar cell devices. Lifetime metrology can also be used to screen new materials as solar cell absorbers. The defining characteristic of MAPbX₃ is the large τ_0 that can be achieved with much lower processing temperatures and source purities than are needed for more typical semiconductors. An emphasis on lifetime metrology would accelerate the search for a Goldilocks material: a solar cell absorber with large τ_0 , an appropriate bandgap, and strong optical absorption that is also phase-stable, non-toxic, and can be manufactured at low cost.¹

ACKNOWLEDGMENTS

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APPENDIX A: DATA PRE-PROCESSING

The amplitude transmission through an air/thin film/substrate structure can be written as²⁵

$$T_{TF} = \frac{2}{1 + n_s + Z_0 \sigma d}. \quad (\text{A1})$$

Z_0 is the impedance of free space. Our substrates are fused quartz with $n_S = 2.13 \pm 0.01$ at 1 THz as measured by THz spectroscopy on bare substrates. The optical pump changes σ , and the other terms in Equation (A1) remain the same. The amplitude transmission to air at the back of the substrate cancels in the ratio $\Delta T/T_0$, and due to the time-domain nature of the experiment, we can ignore multiple reflections within the substrate. We can therefore relate $\Delta T/T_0$ to the relevant material parameters

$$\frac{-\Delta T/T_0}{1 + \Delta T/T_0} = \frac{\sigma_1/\sigma_0}{1 + \frac{1+n_S}{Z_0 d \sigma_0}} = \left(\frac{1}{1 + \frac{1+n_S}{Z_0 d \sigma_0}} \right) \left(\frac{m_h^*}{m_e^*} + 1 \right) \frac{\bar{n}(t)}{p_0}. \quad (\text{A2})$$

These equations are written for a p -type semiconductor. The film conductivity $\sigma(t) = \sigma_0 + \sigma_1$, where σ_0 is the equilibrium value and σ_1 is the excess photoconductivity. The second equality follows from the expression $\sigma_1 = q\mu_e \bar{n} + q\mu_h \bar{p}_1$ and the assumptions that $\bar{n} = \bar{p}_1$ and that $\mu_e/\mu_h = m_h^*/m_e^*$. \bar{p}_1 is the excess majority carrier concentration and μ_e and μ_h are the electron and hole mobility, respectively. In the absence of published measurements of the effective masses, we take $m_h^*/m_e^* = 2$, the average of m_h^*/m_e^* along the crystal axes as calculated by density functional theory.⁵⁴ We assume that the mobilities are constant in time. This is valid because the peak injection levels are always below the level of degeneracy, and because the timescales involved are much longer than typical hot carrier relaxation times. With these assumptions, we use Equation (A2) to calculate $\bar{n}(t)$ from $\Delta T/T_0$.

APPENDIX B: SPATIAL PROFILE OF EXCESS-CARRIERS

The dynamics of excess minority-carriers including generation and recombination are modelled using diffusion equation and appropriate boundary conditions

$$\begin{aligned} \frac{\partial n}{\partial t} &= D \frac{\partial^2 n}{\partial x^2} + G - \frac{n}{\tau}, \\ \frac{\partial n}{\partial x} \Big|_{x=-d/2} &= S n \left(x = -\frac{d}{2} \right), \\ \frac{\partial n}{\partial x} \Big|_{x=d/2} &= -S n \left(x = \frac{d}{2} \right). \end{aligned} \quad (\text{B1})$$

The optical generation is G , the film thickness is, and the interfaces are at $x = \pm d/2$. The film is illuminated from the front surface ($x = -d/2$). We assume that the SRV is the same at front and back surfaces. Although this may be inaccurate in some cases, recombination at the back surface is not relevant in our samples. The geometry is illustrated in Figure 2.

The generation $G(x, t)$ is determined by the reflectivity and absorption coefficient (α) of the sample, the pump fluence (N_0), and the time profile of the pump convoluted with the time resolution of the experiment. The solutions to Equation (B1) therefore include time-dependent generation, rather than assuming a given excess carrier profile at time $t=0$ as a boundary condition. For SnS, this is important

because a non-negligible amount of recombination occurs during the pump pulse. Including time-dependent generation is also useful for modeling other experiments such as quasi-steady-state photoconductivity.

Solutions to Equation (B1) have the form of Equation (3). When calculating the average $\bar{n}(t)$ the sine term disappears, leaving terms of the form $A_j \exp(-(\frac{1}{\tau} + \alpha_j^2 D)t) \cos(\alpha_j x)$. The surface recombination times $\tau_{s,j} = \frac{1}{\alpha_j^2 D}$ satisfy $\tau_{s,j} < t_d/4\pi^2$ for all $j > 1$, where $t_d = d^2/D$ is the diffusion time. Therefore, the TPC data must extend to times $t \gg t_d/4\pi^2$ in order for τ_{eff} to be determined by a single exponential fit to the data. For an ideal experiment with arbitrary sensitivity, this could always be satisfied. However, real experiments have finite sensitivity, and the requirement of collecting data for $t \gg t_d/4\pi^2$ may not be met. The total signal decays no faster than τ_{eff}^{-1} . Therefore, experiments are sensitive at times $t \ll \tau_{\text{eff}}$ and insensitive at times $t \gg \tau_{\text{eff}}$. By combining the known solutions to Equation (B1) with this estimate of experimental sensitivity, we identify parameter spaces within which the spatial distribution of excess-carriers can and cannot be ignored when fitting TPC data.

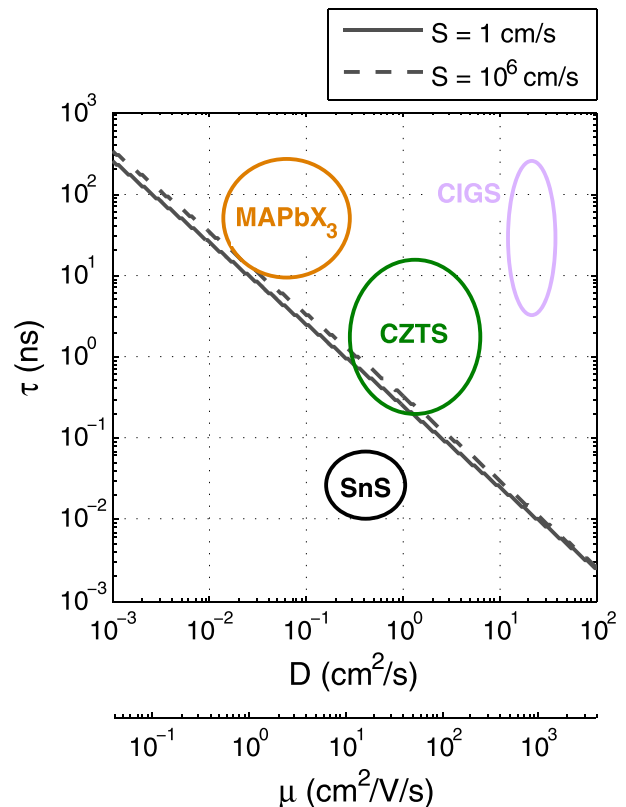


FIG. 6. Parameter spaces on the D - τ plane within which the spatial distribution of excess-carriers can and cannot be ignored when fitting TPC data for fixed film thickness $d = 1 \mu\text{m}$. The grey lines satisfy the condition $\tau_{\text{eff}} = t_d/4\pi^2$ for discrete values of S . The second x-axis shows mobility (μ) at 293 K. For $\tau_{\text{eff}} \gg t_d/4\pi^2$ (upper right) the fundamental mode is easily measured, and the spatial distribution of excess-carriers does not affect the estimation of τ_{eff} . For $\tau_{\text{eff}} \ll t_d/4\pi^2$ (lower left) the data are not well characterized by a single exponential decay, and the spatial distribution of excess-carriers must be considered in order to estimate τ_{eff} . The circles indicate typical parameter spaces for different thin film materials, with the same color scheme as Figure 1.

For $\tau_{\text{eff}} \gg t_d/4\pi^2$, the fundamental mode is easily measured, and the spatial distribution of excess-carriers does not affect the estimation of τ_{eff} . For $\tau_{\text{eff}} \ll t_d/4\pi^2$, the data are not well characterized by a single exponential decay, and the spatial distribution of excess-carriers must be considered in order to estimate τ_{eff} . In Figure 6, we show these parameter spaces in the D - τ plane for discrete values of S and fixed film thickness $d = 1 \mu\text{m}$, which is typical for thin film solar cell absorbers. We also indicate parameter regimes that characterize different absorber materials. For long minority-carrier lifetimes and/or fast diffusion, the spatial distribution does not affect the determination of τ_{eff} (Figure 5(a)). For short minority-carrier lifetimes and/or slow diffusion, the spatial distribution must be explicitly accounted for in order to determine τ_{eff} (Figure 5(b)).

τ_{eff} depends on both bulk and surface recombination (Equation (4)). The exponential decay at long times reflects the minority-carrier lifetime (τ) only for the case of small τ or very well passivated surfaces ($S < 100 \text{ cm/s}$). In Figure 7, we

plot the ratio τ_{eff}/τ as a function of D and τ for discrete values of S and for a fixed film thickness $d = 1 \mu\text{m}$. For wafer-based materials such as Si, there are well-known techniques for passivating the surface ($S < 1 \text{ cm/s}$ can be achieved by immersion in HF) in order to directly measure τ .¹⁴ For thin film materials, this degree of control over surface recombination has not been achieved, and as a result, τ_{eff} is usually dependent on τ , d , D , and S .

APPENDIX C: MINORITY CARRIER RECOMBINATION AT VARIABLE INJECTION CONDITIONS

In Figure 8, we compare model calculations of $\bar{n}(t)$ with and without including the injection-dependence of the minority-carrier lifetime described by Equation (5), using parameters appropriate for a representative sample (TE4). The injection-dependence significantly slows the overall decay and has a corresponding effect on the model for $\bar{n}(t)$ and on the estimate for τ_0 : compare the curve labelled “injection-

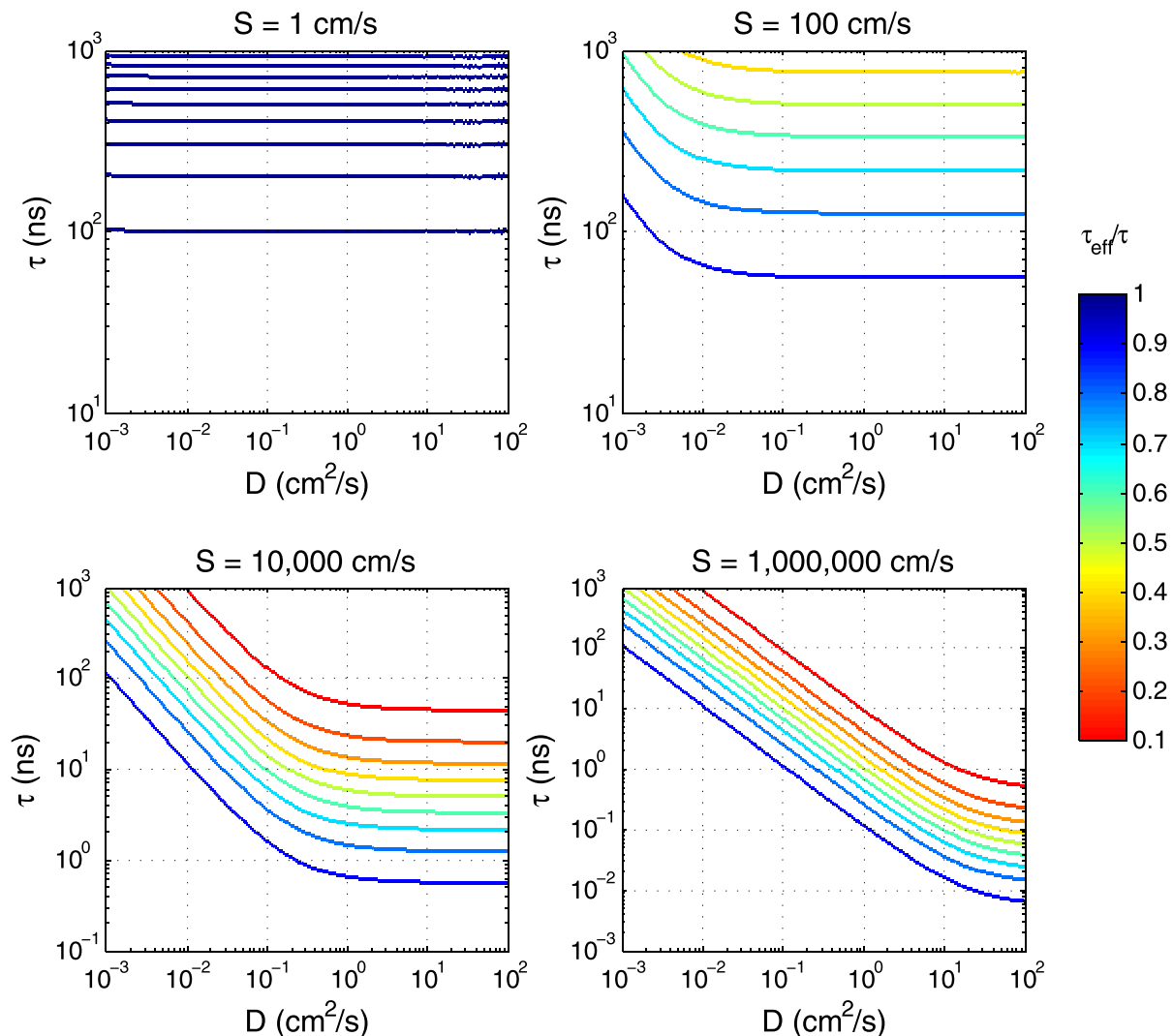


FIG. 7. Ratio of effective lifetime τ_{eff} to the bulk minority-carrier lifetime τ_0 as a function of D and τ for discrete values of S and fixed film thickness $d = 1 \mu\text{m}$. For $\tau_{\text{eff}}/\tau_0 \approx 1$ (blue contours), the minority-carrier lifetime can be estimated from the effective lifetime. For $\tau_{\text{eff}}/\tau_0 < 1$, the effective lifetime is affected by both bulk and surface recombination. For extremely well-passivated surfaces with $S = 1 \text{ cm s}^{-1}$ (upper left plot), τ_{eff} is nearly equal to τ_0 for all values of τ_0 and D . For highly defective surfaces with $S = 1 \times 10^6 \text{ cm s}^{-1}$ (lower right plot), τ_{eff} approaches τ_0 only for small values of τ_0 and D .

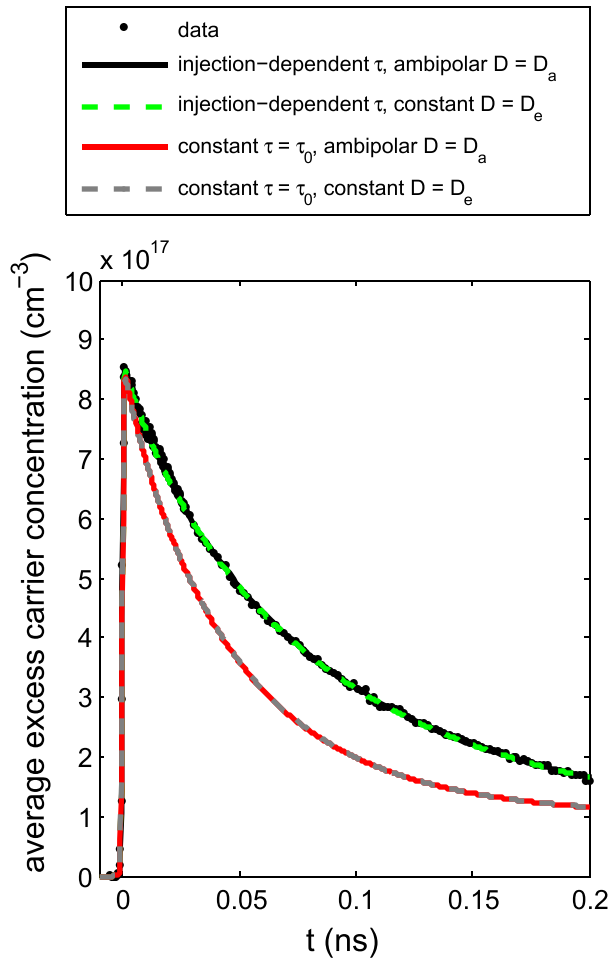


FIG. 8. Effects of high-injection and ambipolar diffusion on the thickness-averaged excess minority-carrier concentration $\bar{n}(t)$. Lines show the solutions to the nonlinear diffusion model, and points are experimental data. The data are for sample TE4 with 800 nm pump wavelength, the same as presented in Figure 2. For this sample $p_0 = 8.07 \times 10^{16} \text{ cm}^{-3}$, and for this dataset the pump fluence $N_0 = 1.01 \times 10^{14} \text{ cm}^{-2}$. Black solid line: model with injection-dependent τ and ambipolar $D = D_a$, as described in Eqs. (4) and (5) and used to generate the results reported here. Green dashed line: model with injection-dependent τ and constant $D = D_e$. Red solid line: model with constant $\tau = \tau_0$ and ambipolar $D = D_a$. Grey dashed line: model with constant $\tau = \tau_0$ and constant $D = D_e$. For all model curves $\tau_0 = 0.069 \text{ ns}$ and $D_e = 0.894 \text{ cm}^2/\text{s}$.

dependent τ , ambipolar $D = D_a$ ” (black solid line) to the curve labelled “constant $\tau = \tau_0$, ambipolar $D = D_a$ ” (red solid line). Without the injection-dependent model, τ_0 would be overestimated by approximately a factor of two.

Surface recombination must also depend on injection conditions because it is also governed by the statistics of trap occupation.⁵⁵ However, this is important only for materials with well-passivated surfaces. For example, $S < 1000$ is readily achieved at the Si/SiO₂ interface, and the excess-carrier concentration at the surface can be large. In this situation, the injection-dependence of S can significantly affect lifetime measurements and solar cell operation.^{55,56} However, for most thin films S is large, and the excess-carrier concentration at the surface is small. For our measurements, we estimate that $n(x = -d/2) < p_0$ holds for all data except at very short times after photoexcitation. Injection-dependence of S would result in a nonlinear dependence of the peak measured injection

(\bar{n}_{MAX}) on the total pump fluence N_0 . We find that \bar{n}_{MAX} is weakly nonlinear for over two orders of magnitude variation in N_0 , from 10^{13} to 10^{15} cm^{-2} . Therefore, it is appropriate to assume a constant value for S .

APPENDIX D: CONSTRAINING THE MINORITY CARRIER DIFFUSIVITY

The assumption that there are no electric fields in the film requires that excess majority- and minority-carriers diffuse together with the ambipolar diffusivity D_a (Ref. 57)

$$D_a = \frac{n+p}{\frac{n}{D_e} + \frac{p}{D_h}} = D_e \frac{p_0 + 2n}{p_0 + n \left(1 + \frac{m_h^*}{m_e^*}\right)}. \quad (\text{D1})$$

D_h and D_e are the bare hole and electron diffusivities and are related to the mobilities by the Einstein relation $D_{h,e} = k_B \Theta \mu_{h,e} / q$. Θ is the temperature. D_a is injection-dependent and introduces another term nonlinear in n to Equation (B1). The effect of including this nonlinearity is illustrated in Figure 8 where we compare the model with and without the injection-dependence of D_a using data and parameters for a representative sample (TE4). For SnS, the injection-dependence of D_a is not strong, and its effect on the model for $\bar{n}(t)$ is negligible: compare the curve labelled “injection-dependent τ , ambipolar $D = D_a$ ” (black solid line) to the curve labelled “injection-dependent τ , constant $D = D_e$ ” (green dashed line).

We constrain the in-plane mobility at THz frequencies to be related by the Einstein relation to the out-of-plane diffusivity. Therefore, the fitting parameter D_e , the minority carrier diffusivity in the low-injection limit, affects the overall scale of the dataset in addition to affecting the TPC decay dynamics. This can be seen by rewriting Equation (A2)

$$\begin{aligned} \bar{n} &= \left(\frac{-\Delta T/T_0}{1 + \Delta T/T_0} \right) \left(1 + \frac{1 + n_S}{Z_0 d \sigma_0} \right) \left(\frac{1}{m_h^*/m_e^* + 1} \right) p_0, \\ &\approx \left(\frac{-\Delta T/T_0}{1 + \Delta T/T_0} \right) \left(\frac{1}{m_h^*/m_e^* + 1} \right) \frac{1 + n_S}{Z_0 d q} \frac{1}{\mu_h}, \\ &= \left(\frac{-\Delta T/T_0}{1 + \Delta T/T_0} \right) \left(\frac{1}{m_h^*/m_e^* + 1} \right) \frac{1 + n_S}{Z_0 d q} \frac{m_h^* k_B \Theta}{m_e^* D_e}. \end{aligned} \quad (\text{D2})$$

The approximation on the second line follows from the fact that $Z_0 d \sigma_0 = 0.0002$ – 0.02 for $1 \mu\text{m}$ thick films with $\sigma_0 = 0.005$ – 0.5 S/cm , which covers our entire sample set. This approximation helps to visualize the relationships between the parameters, but is not necessary to apply this constraint. Equation (D2) shows that the fitting parameter D_e controls the scale of the data $\bar{n}(t)$.

APPENDIX E: SAMPLE HEATING AND THE DATA AT LONG TIMES

At long times, the data $\Delta T/T_0$ are expected to decay exponentially to zero with time constant τ_{eff} . However, our data instead saturate at a finite value $(\Delta T/T_0)_{\text{SAT}}$. In Figure 9, we show representative data for a number of different samples with a fixed pump (400 nm , $11 \mu\text{J/cm}^2$), and in the inset,

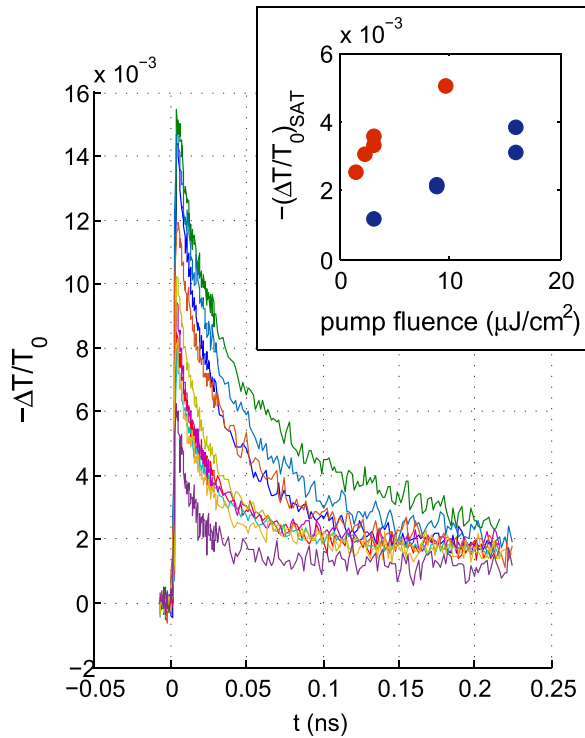


FIG. 9. Saturation of $\Delta T/T_0$ at non-zero values $(\Delta T/T_0)_{\text{SAT}}$ at long times. The main panel shows $\Delta T/T_0$ measured for a 400 nm, $11 \mu\text{J}/\text{cm}^2$ pump. The different colored lines indicate different samples. The transient decay reflects the recombination of excess-carriers, and the size of the peak at short times depends on the sample mobility (Equation (A2)). The saturation at long times is of unknown origin. (Inset) $(\Delta T/T_0)_{\text{SAT}}$ as a function of pump fluence and wavelength for an individual sample (sample TE3). The blue and red points indicated 400 and 800 nm pump, respectively.

we show the dependence of $-(\Delta T/T_0)_{\text{SAT}}$ on pump fluence for a single sample. $(\Delta T/T_0)_{\text{SAT}}$ varies slightly between samples and increases monotonically with pump fluence.

Transient heating can plausibly account for these observations. Here we discuss one such mechanism, the direct heating of the film by the laser pulse. We do not propose this effect as the clear explanation for the observed $(\Delta T/T_0)_{\text{SAT}}$. Rather, we use it to illustrate the existence of transient processes with widely varying timescales, and the challenge of addressing these processes with a limited experimental time window.

A short laser pulse with energy in the range 10^{-5} – 10^{-4} J/cm^2 can raise the temperature of a $1 \mu\text{m}$ SnS film by between 0.1 and 1 K. This can result in a thermal response in $\Delta T/T_0$ on the order of 10^{-3} . Crucially, the timescale on which the film cools to ambient temperature is longer than the timescale for excess-carrier recombination, but is shorter than the experimental repetition rate. Therefore, this thermal effect can be easily mistaken for a long-lived electronic excitation, with characteristic lifetime exceeding the experimental window.

We demonstrate this effect by solving a thermal model of the air/film/substrate system, using parameters appropriate to SnS and fused quartz where available. The SnS heat capacity (C), density (ρ), and thermal conductivity (K) are $45 \text{ J mol}^{-1} \text{ K}^{-1}$, 5.08 g cm^{-3} , and $1.3 \text{ W m}^{-1} \text{ K}^{-1}$, respectively.^{58,59} We hold both the air and the substrate at

ambient temperature (Θ_A). We take the air/film thermal boundary conductance to be $5 \times 10^{-4} \text{ W cm}^{-2} \text{ K}^{-1}$, appropriate for a surface with emissivity of unity.⁶⁰ We take the film/substrate thermal boundary conductance to be $5 \times 10^3 \text{ W cm}^{-2} \text{ K}^{-1}$, as for the Si/SiO₂ interface.⁶¹ We assume that the electronic excitation following the optical pump quickly decays into heat, so that the initial temperature distribution at $t=0$ is $\theta_A + (\alpha Q_0/\rho C)e^{-\alpha(x-d/2)}$, where α is the optical absorption coefficient and Q_0 is the pump energy density. We plot in Figure 10(a) the resulting temperature profile through the film as a function of time. For $t < 1 \mu\text{s}$, there is some redistribution of heat through the film, but little loss to the substrate. The film starts cooling at times $t > 1 \mu\text{s}$. This is simply the thermal diffusion time (t_Θ) for $d=1 \mu\text{m}$ of SnS: the Kelvin diffusivity is $\kappa=K/\rho C=0.0086 \text{ cm}^2 \text{ s}^{-1}$, and $t_\Theta=d^2/\kappa=1 \mu\text{s}$. For times $t < t_\Theta$, the thickness-averaged sample temperature (Θ_S) is nearly equal to $\Theta_A + 0.2 \text{ K}$.

We measured directly the effect of changing temperature on the THz signal. We measured the full THz transmitted waveform through sample TE3 while varying Θ_S using a heating stage and with no pump beam. The amplitude transmission decreased with increasing Θ_S , with no noticeable shift in phase. We use the resulting data to parameterize $\Delta T_\Theta/T_0$ as a function of Θ_S , where $\Delta T_\Theta=T(\Theta_S)-T(\Theta_A)$ and $T_0=T(\Theta_S=\Theta_A)$. This can be combined with the output of thermal simulations to produce an estimate of the signal $\Delta T_\Theta/T_0$ as a function of Q_0 . In Figure 10(b), we show an example of the simulated $\Delta T_\Theta/T_0$ as a function of time for typical experimental parameters. To this we add the TPC signal $\Delta T_{\text{TPC}}/T_0$ calculated using the model described above and material parameters taken from sample TE3. For a material such as SnS with a short minority-carrier lifetime, the timescales for excess-carrier recombination and sample cooling are well separated, making these effects easier to distinguish. For longer-lifetime materials, these timescales may become comparable, which would complicate the analysis. The analysis of thermal effects is made difficult by the fact that the timescale for thermal transients is orders of magnitude longer than the time that can be covered by typical delay stages.

Transient heating of the thin film as described above accounts for a significant fraction of the measured $(\Delta T/T_0)_{\text{SAT}}$. We hypothesize that other thermal transients may also contribute to these observations. This hypothesis can be tested by changing the sequence of visible and THz pulses and by changing the thermal conductivity of the sample environment. For sample TE1 that was measured in vacuum, we see evidence of extended thermal transients on a timescale of minutes. This is consistent with an increase in the thermal time constant of the sample, substrate, and sample holder due to the lack of convective cooling in vacuum. On a practical level, this can be dealt with by increasing the experimental repetition rate so that the sample remains heated for the entire measurement sequence. Measurements extending over much longer time delays would enable $(\Delta T/T_0)_{\text{SAT}}$ to be studied directly and better understood. Unfortunately, this may require that the pump-probe time delay extend to the experimental repetition period of 1 ms or longer, whereas typical delay stages have a maximum extent on the order of 1 ns.

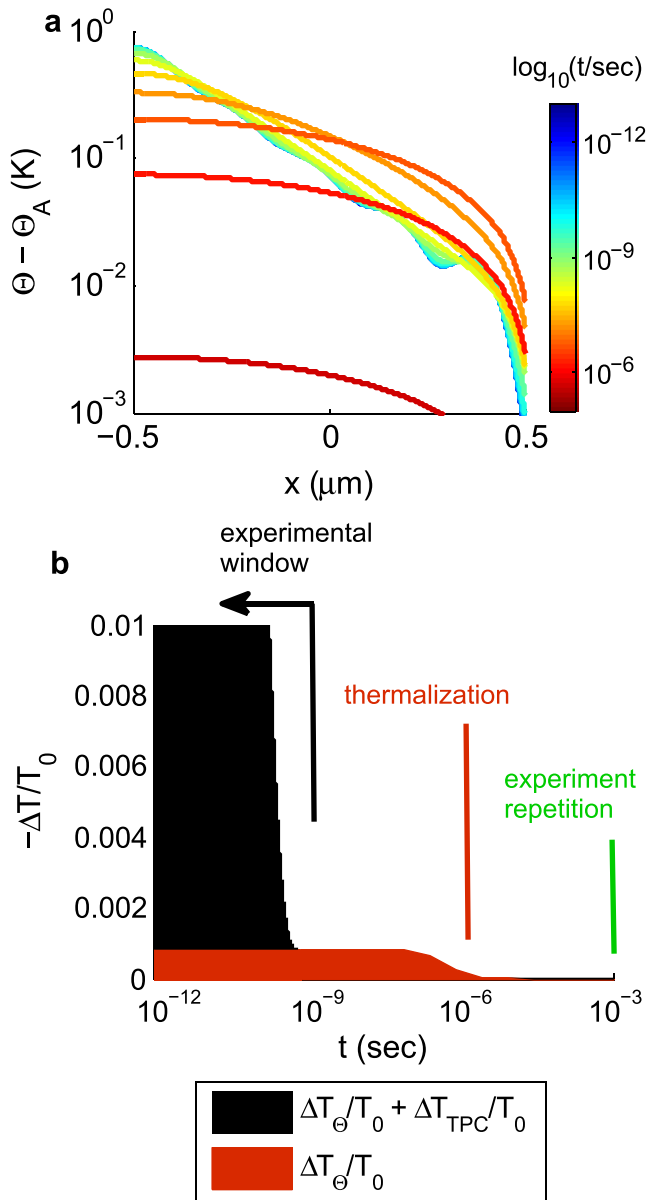


FIG. 10. Effect of transient sample heating on measured $\Delta T/T_0$. (a) Temperature profile $\Theta(x, t)$ through a 1 mm thick SnS film on fused quartz as a function of time (t) after an instantaneous laser pulse that is incident on the surface at $x = -0.5 \mu\text{m}$. The ambient temperature is Θ_A . The simulation is described in the text and the laser pulse has wavelength 800 nm and total energy density $25 \mu\text{J cm}^{-2}$. $\Theta - \Theta_A$ decays quickly to zero for $t \gg t_\Theta = 1 \mu\text{s}$. The oscillations at short times are artifacts due to numerical truncation. (b) We average the temperature rise in (a) through the film thickness and convert it to a thermally induced rise $\Delta T_\Theta/T_0$ (red filled area) using an independent measurement of THz transmission as a function of temperature. For illustration, we add to this thermal transient the photoconductivity signal $\Delta T_{\text{TPC}}/T_0$ that we calculate from the model using parameters typical for sample TE3 and $f=0$ (black filled area). The y-axis is truncated well below the maximum in $\Delta T_{\text{TPC}}/T_0$ in order to emphasize the long transient $\Delta T_\Theta/T_0$, which is similar in magnitude to the measured $(\Delta T/T_0)_{\text{SAT}}$.

We account for $(\Delta T/T_0)_{\text{SAT}}$ by adding to the model a term $\bar{n}_f(t) = f \int_{t_1}^t dt' N(t')$, where f is a fit parameter and $N(t)$ is the time-dependence of the pump fluence such that the total fluence $N_0 = f \int_{t_1}^{t_2} dt' N(t')$. The integration limits t_1 and t_2 cover the full extent of a single pulse. $\bar{n}_f(t)$ expresses our assumption that $(\Delta T/T_0)_{\text{SAT}}$ increases monotonically with

pump fluence and results from processes with an asymmetrical time response. The signal $(\Delta T/T_0)_{\text{SAT}}$ rises as quickly as the pump arrives but decays on a timescale much longer than the experimental time window. The f parameter is relatively constant across our entire sample set for a fixed set of pump wavelength, total fluence, and measurement laboratory. The addition of this f parameter to the model is an unfortunate necessity and reflects our incomplete understanding of the electrical and thermal response of our samples and the experimental apparatus. The extent to which $(\Delta T/T_0)_{\text{SAT}}$ results from long-lived electronic excitations in the sample such as surface traps could be tested by using varying temperature or an infrared bias light to de-trap charges during the TPC measurements.

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